



Recent improvements in OPM Flow well handling

Stein Krogstad, SINTEF Digital

Why solve well-equations locally?



- Often more non-linear dynamics in wells than in reservoir
 - Keep number of globally coupled (costly) iterations to minimum
- Handle logic and constraints for groups and network
 - Keep number of globally coupled (costly) iterations to minimum
- Potentials
 - Solution of local well equation by definition

Local well-equations: System of equations resulting from treating reservoir states as constants.

Local well-equations – default behavior in Flow



• Solve well equations for a given fixed control value and mode

Possible drawbacks:

- Given mode/value might not be the most restrictive
 - Wasted iterations
- Given mode/value might not be feasible
 - Convergence failure
- In combination with group control / network, above bullet-points may cause additional problems (control oscillations)

Local well-equations with control mode/status switching

Aim: Local well solve should always converge to the most restrictive mode and/or status

Enabled by:

--local-well-solve-control-switching = true

- both standard- and multisegment wells
- potential calculations
- operability checks

For each local iteration

- 1. Update mode and status
 - *if well is (temporarily) stopped, check if conditions allow reopening, and update status*
 - otherwise
 - if well can't operate, (temporarily) stop
 - otherwise, check well constraints and if violated, switch mode
- 2. Solve and update well state
- 3. Check convergence

Local well-equations with control mode/status switching

Results:

- Increasing advantage with increasing model/well model complexity
- Typically, very valuable in prediction mode (wells stopping/re-opening)

BUT:

• Not sufficiently robust for THPcontrolled wells





For efficiency, local well-solves use simplified check for THP-operability

• may still run into problems for *slightly* inoperable cases

Default IPR computation in flow:

- based on connection rates at bhp=0,
- only *valid* approximation for nearly linear well-equations
- not really used





Implicit approach:

Compute $\frac{dq}{dBHP}$ for current well-state using implicit differentiation

- requires one linear solve of well system
- assumes converged well-equations
- accuracy dependent on well convergence tolerance









Results:

- Typically makes little difference for simple cases
- Robust handling of THP-controlled wells needed for some *difficult* cases
 - prevents excessive time-step cuts and/or failures
- Extra machinery (except stability checks) only kicks in for special situations, so virtually no added cost

Concluding remarks



- Several enhancements for more robust well handling triggered by real field cases
- Largest additions related to local well-solves and robust THPtreatment
- With larger and more complex models, all that can go wrong eventually will go wrong

Possible further uses of implicit IPR:

- Semi-implicit group control
 - avoid oscillations
- Semi-implicit networks
 - improve convergence/runtime





Well equations with bhp-control:

$$E(x,p_w)=0,$$

where x are well-unknowns and p_w is bhp control-value. We have

$$D_{p_{w}}E = \frac{\partial E}{\partial p_{w}} + \frac{\partial E}{\partial x}D_{p_{w}}x = 0,$$

SO

$$D_{p_{w}}x = -\frac{\partial E^{-1}}{\partial x}\frac{\partial E}{\partial p_{w}}$$

Want to find $\frac{dq}{dp_w}$ for rates q: $\frac{dq}{dp_w} = \frac{\partial q}{\partial p_w} + \frac{\partial q}{\partial x} D_{p_w} x$ $= \frac{\partial q}{\partial p_w} - \frac{\partial q}{\partial x} \frac{\partial E^{-1}}{\partial x} \frac{\partial E}{\partial p_w}$



$$\frac{dq}{dp_w} = \frac{\partial q}{\partial p_w} - \frac{\partial q}{\partial x} \frac{\partial E^{-1}}{\partial x} \frac{\partial E}{\partial p_w}$$

- Control value not present in formulation of q, so $\frac{\partial q}{\partial p_w} = 0$.
- $\frac{\partial E}{\partial p_w}$ is zero except for a -1 at position of control equation
- $\frac{\partial q}{\partial x}$ obtained from AD-version of rates

1. Solve linear system
$$\frac{\partial E}{\partial x} v = \frac{\partial E}{\partial p_w}$$

2. Assemble $\frac{dq}{dp_w} = -\frac{\partial q}{\partial x} v$