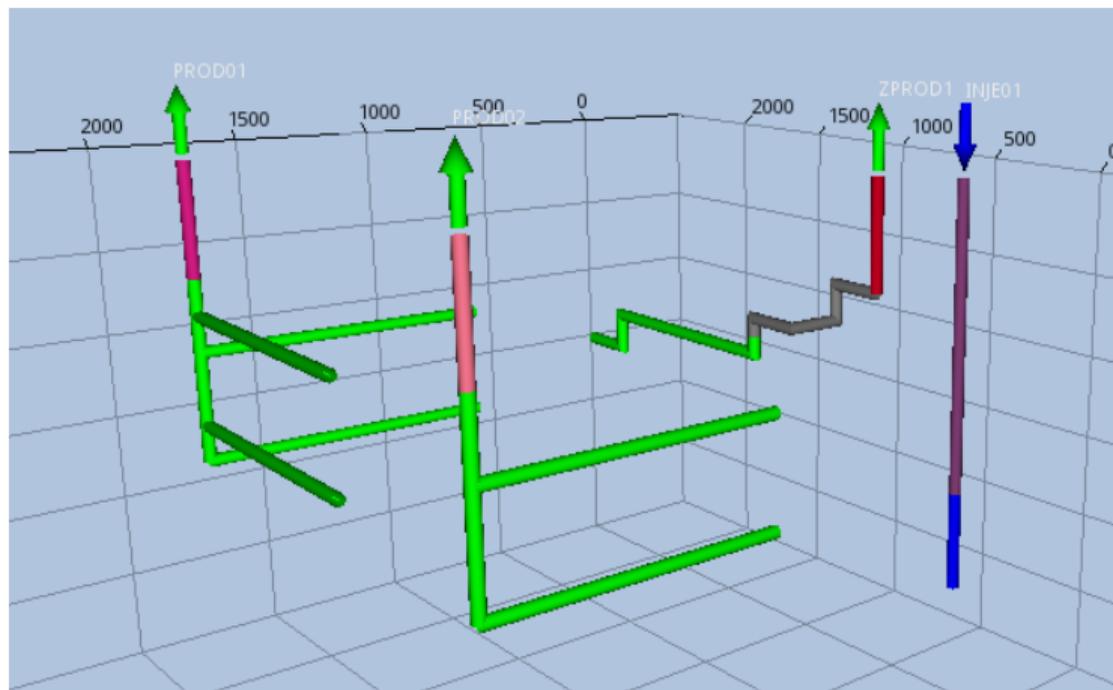


# Parallelization of Multisegment Wells: Enhancing simulation flexibility

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May 27th, 2025

# What are multisegment wells?



- Partitions are critical for the performance!
- The new default partitioner handles well info better → performance improvement!
- Before: Partitions had to keep multisegment wells on one process.
- With distributed multisegment wells: Partitions can be independent of the wells.
- Enable with `--allow-distributed-wells=true`.
- Spoiler<sup>1</sup>: The well-independent version of the new default partitioner slightly outperforms the well-dependent one!

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<sup>1</sup>for the cases I have tested

# Steps to parallelize multisegment wells



- A Linear system solved in each timestep in flow, Schur complement
- B Equations and resulting part of the linear system for standard and multisegment wells
- C Linear system for multisegment wells in parallel
- D Performance results
- E Outlook

## A: Linear system

- reservoir + well equations define a large system of nonlinear equations

$$R(x) = \vec{0}$$

$$\dim(x) = \dim(R(x)) = \underbrace{\# \text{grid cells} \cdot \# \text{primary variables}^1}_{\# \text{reservoir unknowns}} + \underbrace{\# \text{wells} \cdot \# \text{unknowns per well}}_{\# \text{well unknowns}}$$

- solve  $R(x) = \vec{0}$  using a Newton-Raphson type method, i.e., in each iteration: calculate Jacobian  $J(\cdot) \in \mathbb{R}^{\dim(x) \times \dim(x)}$  of  $R$  and solve

$$J(x_n)(x_{n+1} - x_n) = -R(x_n)$$

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<sup>1</sup>one primary variable for each phase, so 3 primary variables for a three-phase black oil system

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calculate Jacobian  $J(\cdot) \in \mathbb{R}^{\dim(x) \times \dim(x)}$  of  $R$  and solve

$$J(x_n)x_{n+1} = J(x_n)x_n - R(x_n)$$

# A: Linear system

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$$J(x_n)x_{n+1} = r_n$$

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- reservoir + well equations define a large system of nonlinear equations

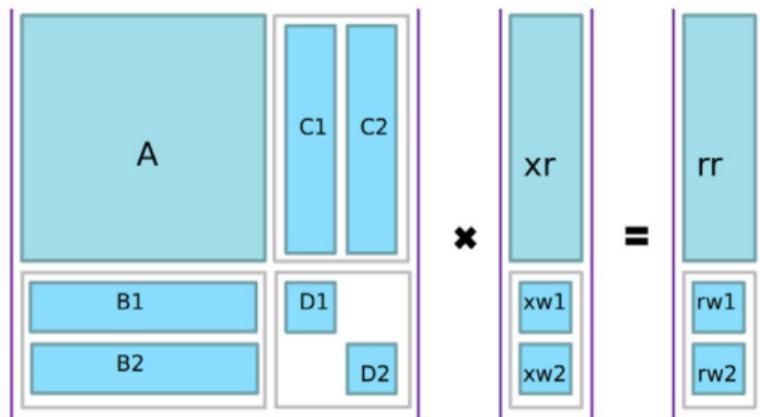
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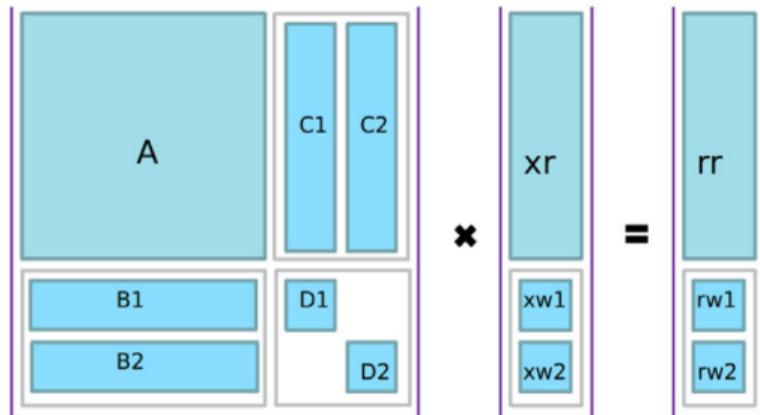
$$\begin{pmatrix} A & C \\ B & D \end{pmatrix} \begin{pmatrix} x_{\text{reservoir}} \\ x_{\text{wells}} \end{pmatrix} = \begin{pmatrix} r_{\text{reservoir}} \\ r_{\text{wells}} \end{pmatrix}$$

# A: Linear system



- $A$ : Jacobian of reservoir equations w.r.t. reservoir unknowns
- $B_j, C_j, D_j$  for each well,  $j = 1, \dots, \#\text{wells}$
- $B_j$ : Jacobian of equations for well  $j$  w.r.t. reservoir unknowns
- $C_j$ : Jacobian of reservoir equations w.r.t. unknowns of well  $j$
- $D_j$ : Jacobian of equations for well  $j$  w.r.t. unknowns of well  $j$

# A: Linear system



- Do not solve the whole system

$$\begin{pmatrix} A & C_1 & C_2 & \dots \\ B_1 & D_1 & & \\ B_2 & & D_2 & \\ \vdots & & & \ddots \end{pmatrix} \cdot \begin{pmatrix} x_r \\ x_{w_1} \\ x_{w_2} \\ \vdots \end{pmatrix} = \begin{pmatrix} r_r \\ r_{w_1} \\ r_{w_2} \\ \vdots \end{pmatrix}$$

as one, instead:

- For  $x_r$  solve

$$\left( A - \sum_{j=1}^{\#wells} C_j D_j^{-1} B_j \right) x_r = r_r - \sum_{j=1}^{\#wells} C_j D_j^{-1} r_{w_j}.$$

- For each  $x_{w_j}$ , solve the small system

$$x_{w_j} = D_j^{-1} (r_{w_j} - B_j x_r).$$

# Steps to parallelize multisegment wells



- A Linear system solved in each timestep in flow, Schur complement
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## B: Well equations for a standard well

- one conservation equation per phase  $\alpha$ :

$$\underbrace{\frac{A_\alpha - A_\alpha^0}{\Delta t}}_{A_\alpha = \text{amount of phase } \alpha \text{ in the wellbore}} + \underbrace{Q_\alpha}_{\text{flow rate of phase } \alpha} - \sum_{i=1}^{\text{connections of the well}} \underbrace{q_{\alpha,i}}_{\text{flow rate of phase } \alpha \text{ through connection } i} = 0$$

- for a three-phase black oil system:  $\alpha \in \{\text{water, oil, gas}\} = \{w, o, g\}$
- one control equation, e.g. for a prescribed bottom hole pressure:

$$p_{bhp} - p_{bhp}^{\text{target}} = 0$$

- unknowns for each well for a three-phase black oil system:

$$\underbrace{Q_t}_{\text{weighted total flow rate}}, \quad \underbrace{F_w, F_g}_{\text{weighted fractions of water and gas}} \quad \text{and} \quad p_{bhp}$$

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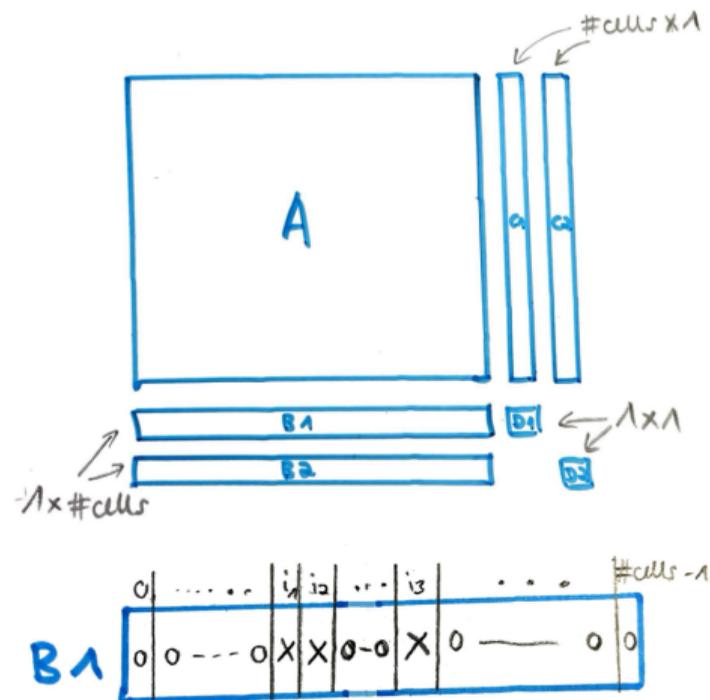
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- unknowns for each well for a three-phase black oil system:

$$\underbrace{Q_t(Q_w, Q_o, Q_g)}_{\text{weighted total flow rate}}, \underbrace{F_w(Q_t, Q_w), F_g(Q_t, Q_g)}_{\text{weighted fractions of water and gas}} \text{ and } p_{bhp}$$

→ four equations and four unknowns per standard well

## B: Linear system for standard wells for 3 phases



- $A$  is a  $\#cells \times \#cells$  BCRS-matrix<sup>1</sup>, inner matrices are  $3 \times 3$
- $B_j$  is a  $1 \times \#cells$  BCRS-matrix, inner matrices are  $4 \times 3$
- $C_j$  is a  $\#cells \times 1$  BCRS-matrix, inner matrices are  $3 \times 4$
- $B_j$  and  $C_j$  only contain entries for the cells that are perforated by the well  $j$
- $B_j$  and  $C_j^T$  have same sparsity pattern
- $D_j$  is a  $1 \times 1$  BCRS-matrix, inner matrix is  $4 \times 4$

<sup>1</sup>BCRS = Blocked Compressed Row Storage collection of small dense inner matrices

## B: Well equations for a standard → multisegment well



- one conservation equation per phase  $\alpha$  (water, oil, gas) :

$$\underbrace{\frac{A_\alpha - A_\alpha^0}{\Delta t}}_{A_\alpha = \text{amount of phase } \alpha \text{ in the wellbore}} + \underbrace{Q_\alpha}_{\text{flow rate of phase } \alpha} - \sum_{i=1}^{\text{connections}} \underbrace{q_{\alpha,i}}_{\text{flow rate of phase } \alpha \text{ through connection } i} = 0$$

- one control equation for the top segment, e.g. for a prescribed bottom hole pressure:

$$p_{bhp} - p_{bhp}^{\text{target}} = 0$$

- unknowns for each standard well for a three-phase black oil system:

$$Q_t(Q_w, Q_o, Q_g), F_w(Q_t, Q_g), F_g(Q_t, Q_g) \text{ and } p_{bhp}$$

→ four equations and four unknowns per standard well

## B: Well equations for a multisegment well

- one conservation equation per phase  $\alpha$  (water, oil, gas) and per segment  $n$ :

$$\underbrace{\frac{A_{\alpha,n} - A_{\alpha,n}^o}{\Delta t}}_{A_{\alpha} = \text{amount of phase } \alpha \text{ in the segment } n} + \underbrace{Q_{\alpha,n}}_{\text{flow rate of phase } \alpha \text{ in segment } n} - \sum_{i=1}^{\text{connections of segment } n} \underbrace{q_{\alpha,i}}_{\text{flow rate of phase } \alpha \text{ through connection } i} - \sum_{i=1}^{\text{inlets of segment } n} \underbrace{Q_{\alpha,i}}_{\text{flow rate of phase } \alpha \text{ in segment } i} = 0$$

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- one control equation for the top segment, e.g. for a prescribed bottom hole pressure:

$$p_{bhp} - p_{bhp}^{target} = 0$$

- one equation for all other segments with the pressure relationship to the outlet segment:

$$p_n - p_{\text{outlet of } n} - (\text{pressure drop between segment } n \text{ and its outlet}) = 0$$

- unknowns for each standard well for a three-phase black oil system:

$$Q_t(Q_w, Q_o, Q_g), F_w(Q_t, Q_g), F_g(Q_t, Q_g) \text{ and } p_{bhp}$$

→ four equations and four unknowns per standard well

## B: Well equations for a multisegment well

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- one equation for all other segments with the pressure relationship to the outlet segment:

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- unknowns for each multisegment well for a three-phase black oil system:

$$Q_{t,n}(Q_{w,n}, Q_{o,n}, Q_{g,n}), F_{w,n}(Q_{t,n}, Q_{g,n}), F_{g,n}(Q_{t,n}, Q_{g,n}) \text{ and } p_{bhp}, p_n (n \neq \text{top segment})$$

→ four equations and four unknowns per standard well

## B: Well equations for a **multisegment well**

- one conservation equation per phase  $\alpha$  (water, oil, gas) and per segment  $n$ :

$$\underbrace{\frac{A_{\alpha,n} - A_{\alpha,n}^o}{\Delta t}}_{A_{\alpha} = \text{amount of phase } \alpha \text{ in the segment } n} + \underbrace{Q_{\alpha,n}}_{\text{flow rate of phase } \alpha \text{ in segment } n} - \sum_{i=1}^{\text{connections of segment } n} \underbrace{q_{\alpha,i}}_{\text{flow rate of phase } \alpha \text{ through connection } i} - \sum_{i=1}^{\text{inlets of segment } n} \underbrace{Q_{\alpha,i}}_{\text{flow rate of phase } \alpha \text{ in segment } i} = 0$$

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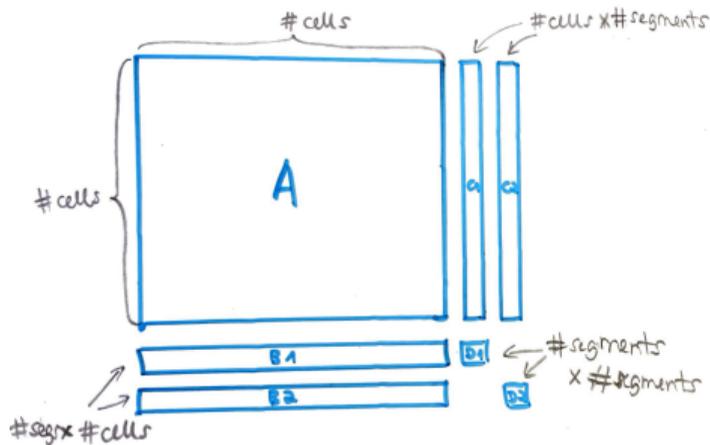
$$p_n - p_{\text{outlet of } n} - (\text{pressure drop between segment } n \text{ and its outlet}) = 0$$

- unknowns for each **multisegment well** for a three-phase black oil system:

$$Q_{t,n}(Q_{w,n}, Q_{o,n}, Q_{g,n}), F_{w,n}(Q_{t,n}, Q_{g,n}), F_{g,n}(Q_{t,n}, Q_{g,n}) \text{ and } p_{bhp}, p_n (n \neq \text{top segment})$$

→ four equations and four unknowns per segment of a multisegment well

# B: Linear system for multisegment wells for 3 phases



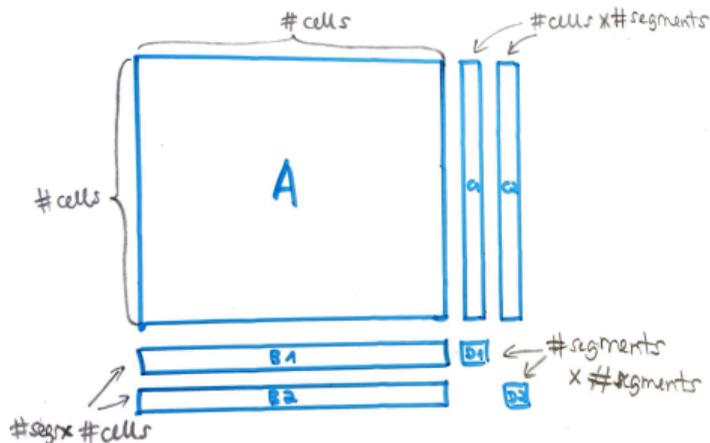
- $A$  is a  $\#cells \times \#cells$  BCRS-matrix, inner matrices is  $3 \times 3$
- $B_j$  is a  $\#segments \times \#cells$  BCRS-matrix, inner matrices are  $4 \times 3$
- $C_j$  is a  $\#cells \times \#segments$  BCRS-matrix, inner matrices are  $3 \times 4$
- $B_j$  and  $C_j$  contain entries for the cells that are perforated by the well  $j$
- $B_j$  and  $C_j^T$  have the same sparsity pattern
- standard wells: one row, all entries are in that one row
- multisegment wells:  $\#segments$  rows, each row has as many entries as the segment has perforations

$B_1$

0	...	$i_1$	$i_2$	...	$i_3$				$\#cells-1$
0	0	-0	X	0	0-0	0	0	-0	0
0	0	-0	0	X	0-0	0	0	-0	0
0	0	-0	0	0	0-0	X	0	-0	0

} # segments

# B: Linear system for multisegment wells for 3 phases

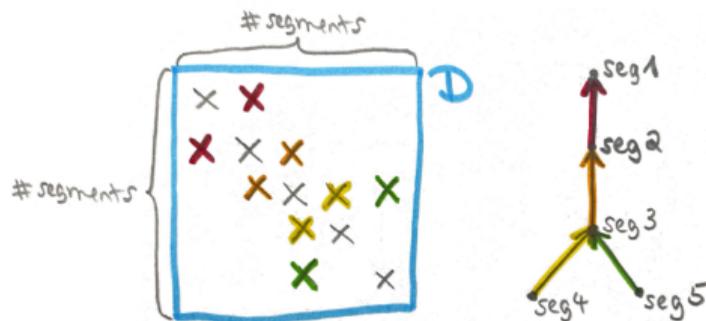


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$B_1$

	0	...	$i_1$	...	$i_2$	...	$i_3$	$i_4$	...	$i_5$	...	$\#cells$
seg1	0		0		0		0	0		0		0
seg2	0		x		0		0	0		0		0
seg3	0	0		0	x		0	0	0	0		0
seg4	0		0		0		x	x		0		0
seg5	0		0		0		0	0		x		0

## B: Linear system for multisegment wells for 3 phases



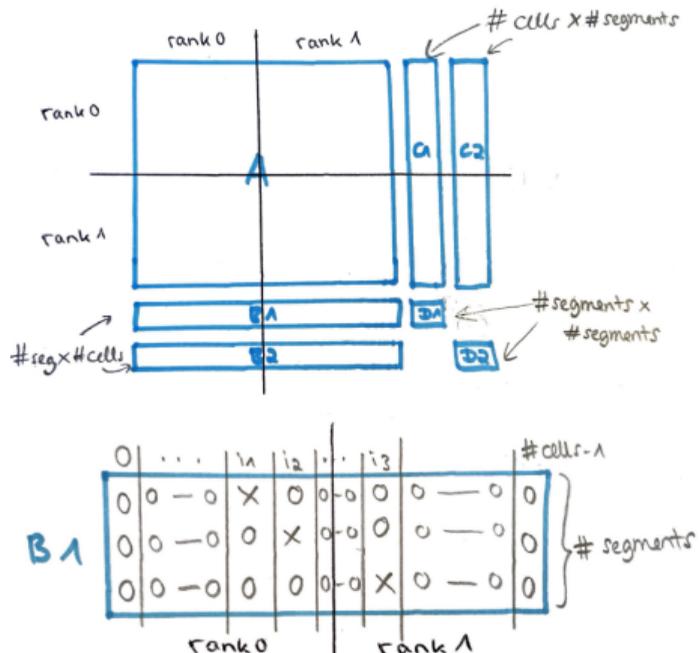
- $D_j$  is a  $\#segments \times \#segments$  BCRS-matrix, inner matrices are  $4 \times 4$
- $D_j$  contains entries on the diagonal and for all connections of the multisegment well
- $D_j$  is generally **not** symmetric, only the sparsity pattern is symmetric

# Steps to parallelize multisegment wells



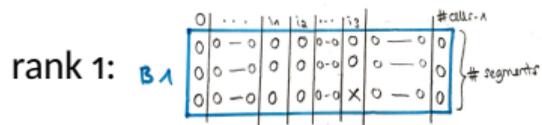
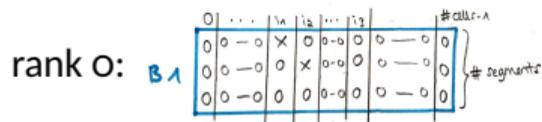
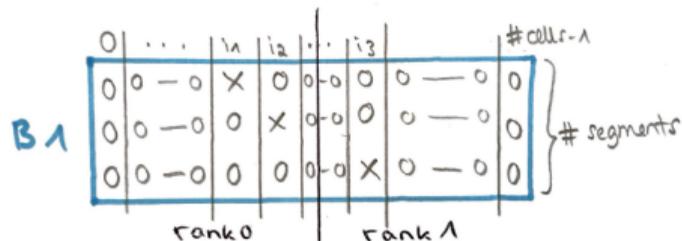
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# C: Linear system for multisegment wells in parallel



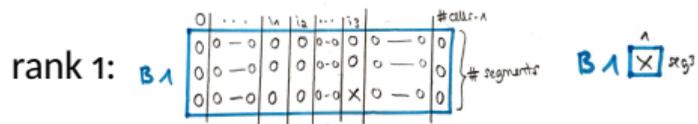
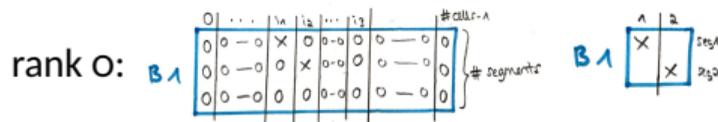
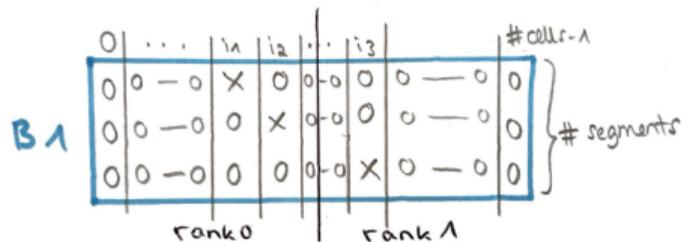
- Each process knows only its own parts of  $B_j$  and  $C_j$ , no overlap!
- $D_j$ ,  $x_{w_j}$ , and  $r_{w_j}$  are shared by all processes linked to the same well.
- Assembling  $B_j$ ,  $C_j$ ,  $D_j$ , and  $r_{w_j}$  requires **communication**, since entries depend on **all** perforations (e.g., pressure differences, averages, maxima, ...).
- One communicator per well!

# C: Linear system for multisegment wells in parallel



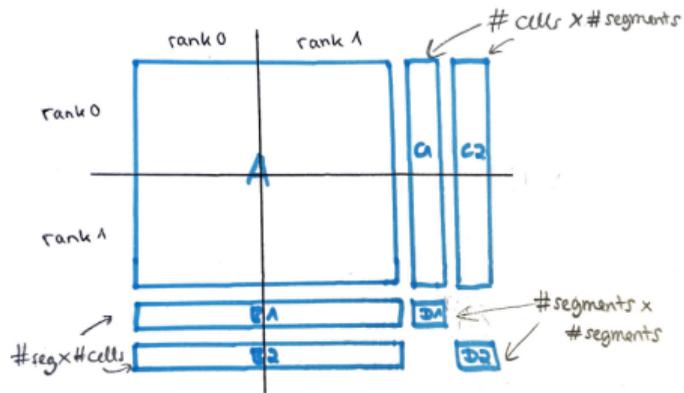
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# C: Linear system for multisegment wells in parallel



Recall the Schur complement approach:

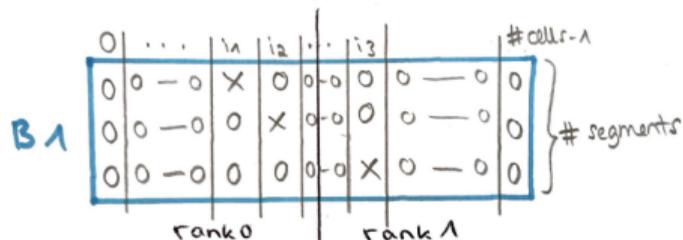
- For each  $x_{w_j}$ , solve the small system

$$x_{w_j} = D_j^{-1} (r_{w_j} - B_j x_r).$$

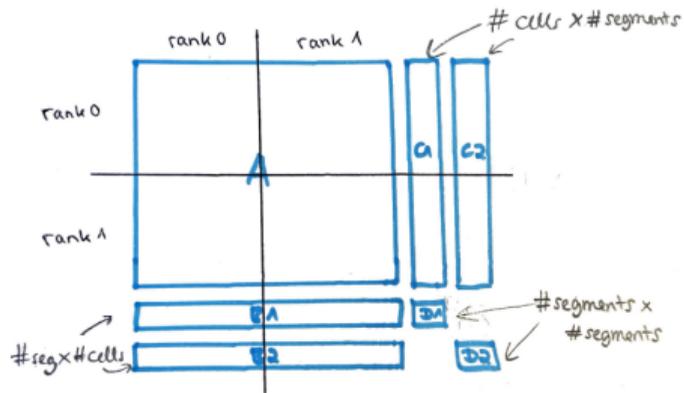
- For  $x_r$ , iteratively solve

$$\left( A - \sum_{j=1}^{\#wells} C_j D_j^{-1} B_j \right) x_r =$$

$$r_r - C_j D_j^{-1} r_{w_j}.$$



# C: Linear system for multisegment wells in parallel



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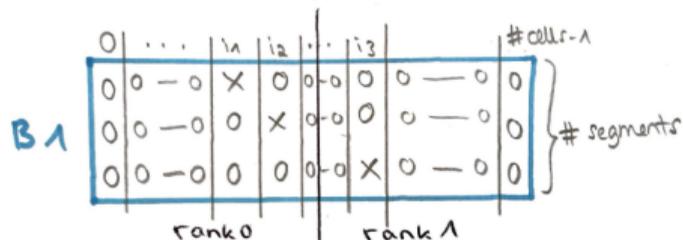
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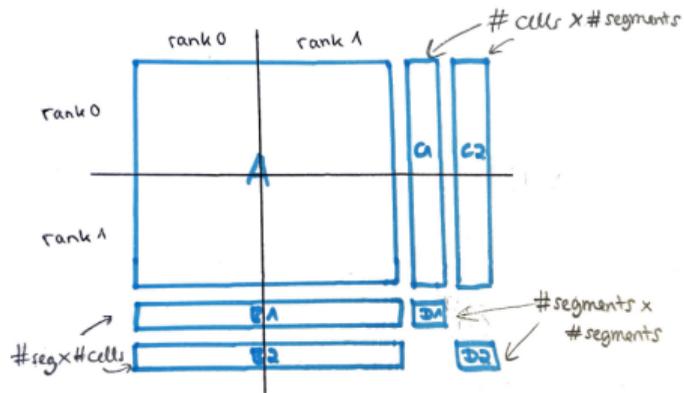
- For  $x_r$ , iteratively solve

$$A \cdot x_r - \sum_{j=1}^{\#wells} C_j D_j^{-1} B_j \cdot x_r =$$

$$r_r - C_j D_j^{-1} r_{w_j}.$$



# C: Linear system for multisegment wells in parallel



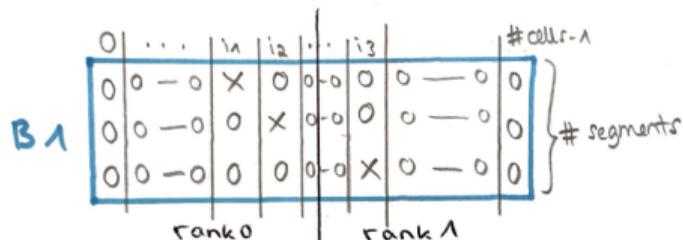
Recall the Schur complement approach:

- For each  $x_{w_j}$ , solve the small system

$$x_{w_j} = D_j^{-1} \left( r_{w_j} - \sum_{k=1}^{\text{all ranks of well } j} (B_j)_{|k} (x_r)_{|k} \right).$$

- For  $x_r$ , iteratively solve

$$A_{|k} \cdot (x_r)_{|k} - \sum_{j=1}^{\text{\#wells}} (C_j)_{|k} D_j^{-1} \left( \sum_{k=1}^{\text{all ranks of well } j} (B_j)_{|k} (x_r)_{|k} \right) = (r_r)_{|k} - \sum_{j=1}^{\text{\#wells}} (C_j)_{|k} D_j^{-1} r_{w_j}.$$



## C: Linear system for multisegment wells in parallel

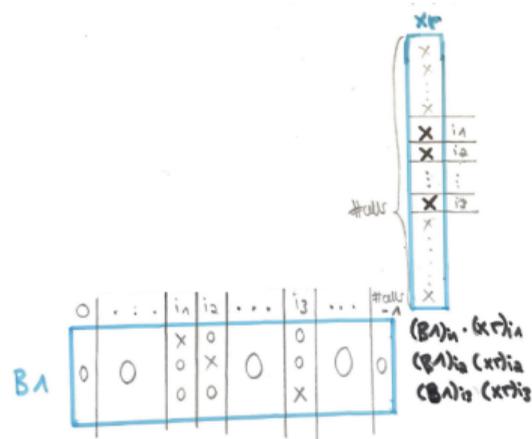


$$x_{w_j} = D_j^{-1} \left( r_{w_j} - \sum_{k=1}^{\text{all ranks of well } j} (B_j)_{|k} (x_r)_{|k} \right) \quad \Bigg| \quad A_{|k} \cdot (x_r)_{|k} - \sum_{j=1}^{\text{\#wells}} (C_j)_{|k} D_j^{-1} \left( \sum_{k=1}^{\text{all ranks of well } j} (B_j)_{|k} (x_r)_{|k} \right) = (r_r)_{|k} - \sum_{j=1}^{\text{\#wells}} (C_j)_{|k} D_j^{-1} r_{w_j}$$

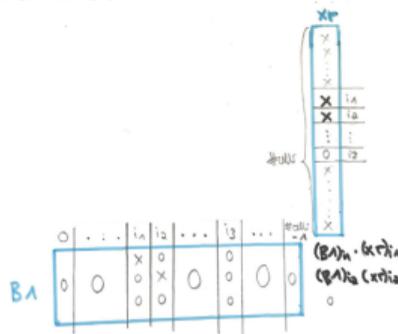
Where is communication needed when multiplying with  $B, D^{-1}, C$ ?

# C: Multiplying with B

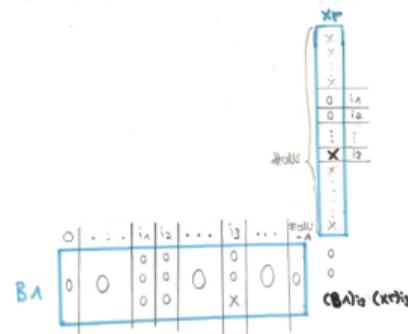
$$x_{w_j} = D_j^{-1} \left( r_{w_j} - \sum_{k=1}^{\text{all ranks of well } j} (B_j)_{|k} (x_r)_{|k} \right) \quad \Bigg| \quad A_{|k} \cdot (x_r)_{|k} - \sum_{j=1}^{\text{\#wells}} (C_j)_{|k} D_j^{-1} \left( \sum_{k=1}^{\text{all ranks of well } j} (B_j)_{|k} (x_r)_{|k} \right) = (r_r)_{|k} - \sum_{j=1}^{\text{\#wells}} (C_j)_{|k} D_j^{-1} r_{w_j}$$



rank 0:



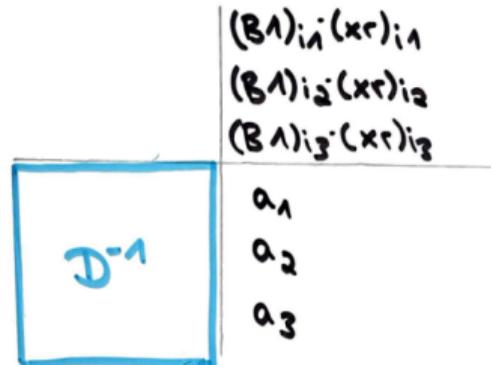
rank 1:



→ Communicate to get the full vector  $B \cdot x_r$  on all ranks perforated by that well!

# C: Multiplying with $D^{-1}$

$$x_{w_j} = D_j^{-1} \left( r_{w_j} - \sum_{k=1}^{\text{all ranks of well } j} (B_j)_{|k} (x_r)_{|k} \right) \quad \Bigg| \quad A_{|k} \cdot (x_r)_{|k} - \sum_{j=1}^{\text{\#wells}} (C_j)_{|k} D_j^{-1} \left( \sum_{k=1}^{\text{all ranks of well } j} (B_j)_{|k} (x_r)_{|k} \right) = (r_r)_{|k} - \sum_{j=1}^{\text{\#wells}} (C_j)_{|k} D_j^{-1} r_{w_j}$$

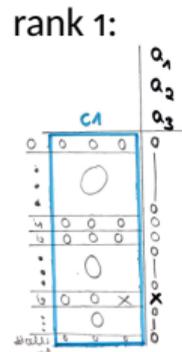
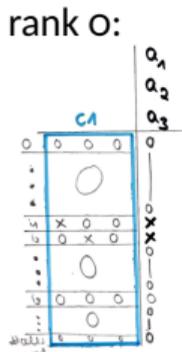
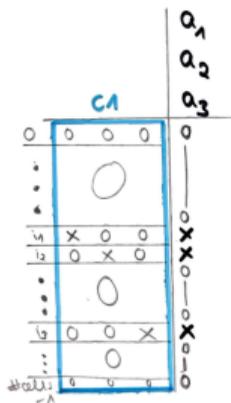


→ Calculate  $D_j^{-1} \cdot (B \cdot x_r)$  and  $D_j^{-1} \cdot r_{w_j}$  on each rank!

→ No communication needed, because  $D_j$ ,  $(B \cdot x_r)$  and  $r_{w_j}$  are the same across all ranks of well  $j$ !

# C: Multiplying with C

$$x_{w_j} = D_j^{-1} \left( r_{w_j} - \sum_{k=1}^{\text{all ranks of well } j} (B_j)_{|k} (x_r)_{|k} \right) \quad \Bigg| \quad A_{|k} \cdot (x_r)_{|k} - \sum_{j=1}^{\text{\#wells}} (C_j)_{|k} D_j^{-1} \left( \sum_{k=1}^{\text{all ranks of well } j} (B_j)_{|k} (x_r)_{|k} \right) = (r_r)_{|k} - \sum_{j=1}^{\text{\#wells}} (C_j)_{|k} D_j^{-1} r_{w_j}$$



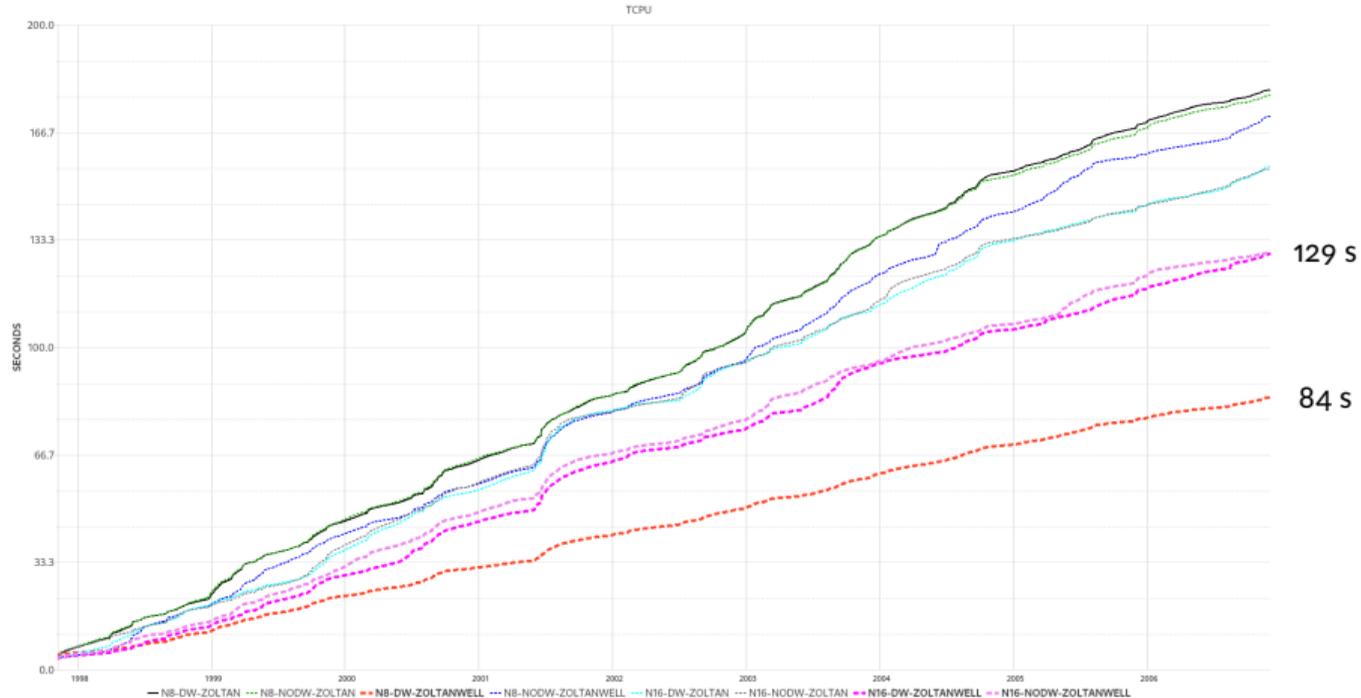
→ Multiplication with  $(C_j)_{|k}$  will automatically reduce to rank k!

# Steps to parallelize multisegment wells



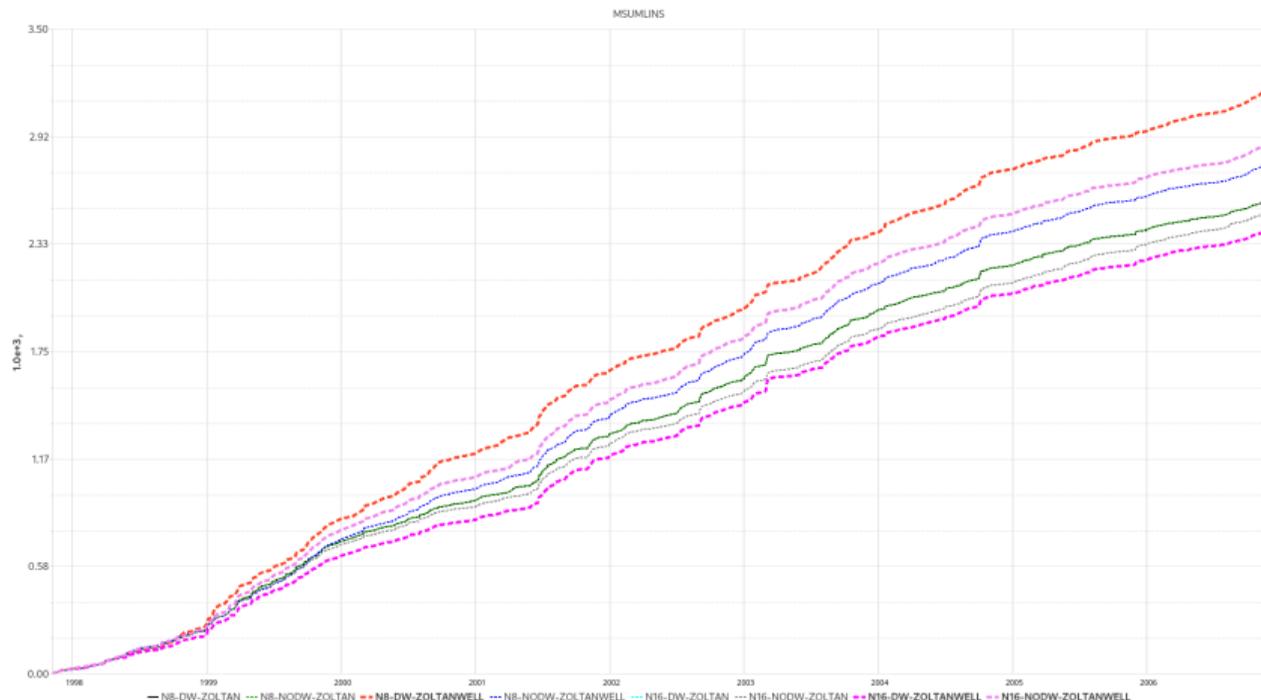
- A Linear system solved in each timestep in flow, Schur complement
- B Equations and resulting part of the linear system for standard and multisegment wells
- C Linear system for multisegment wells in parallel
- D Performance results
- E Outlook

# D: opm-tests/norne/NORNE\_ATW2013.DATA



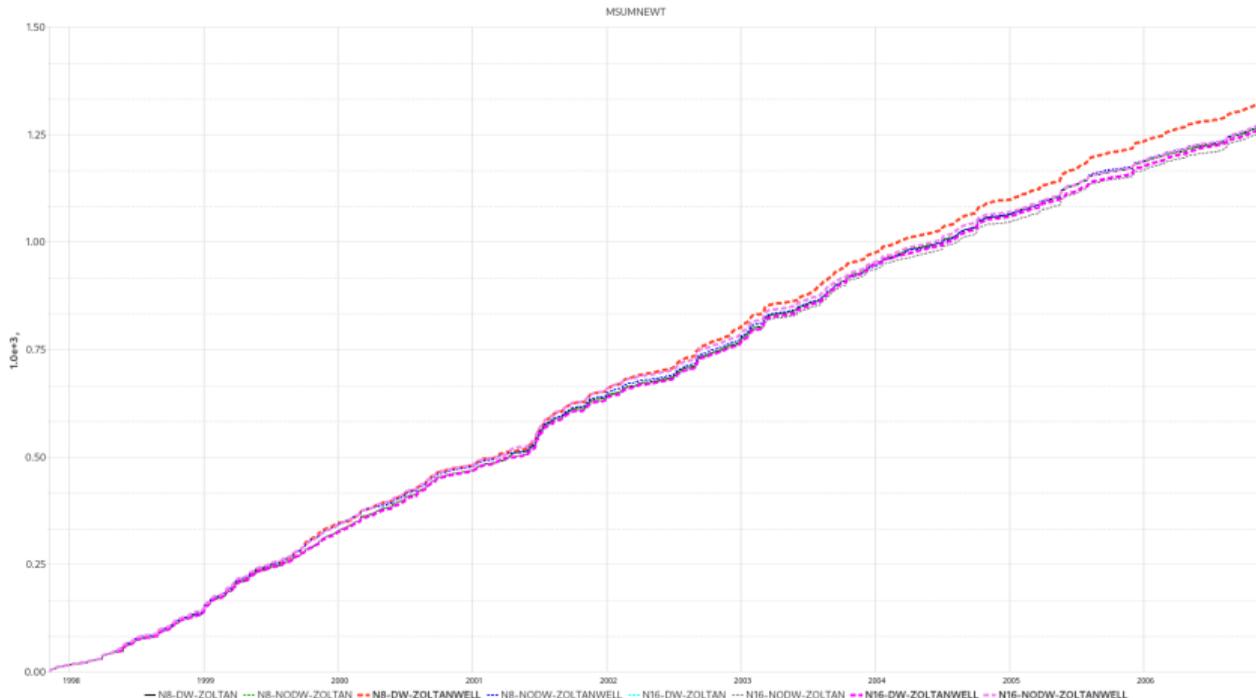
- 8|16 procs, --allow-distributed-wells=true|false --partition-method=zoltan|zoltanwell --allow-splitting-inactive-wells=true  
- Run on a machine with 32 cores, 64 threads, 4.55 GHz max frequency, 128 GB RAM.

# D: opm-tests/norne/NORNE\_ATW2013.DATA



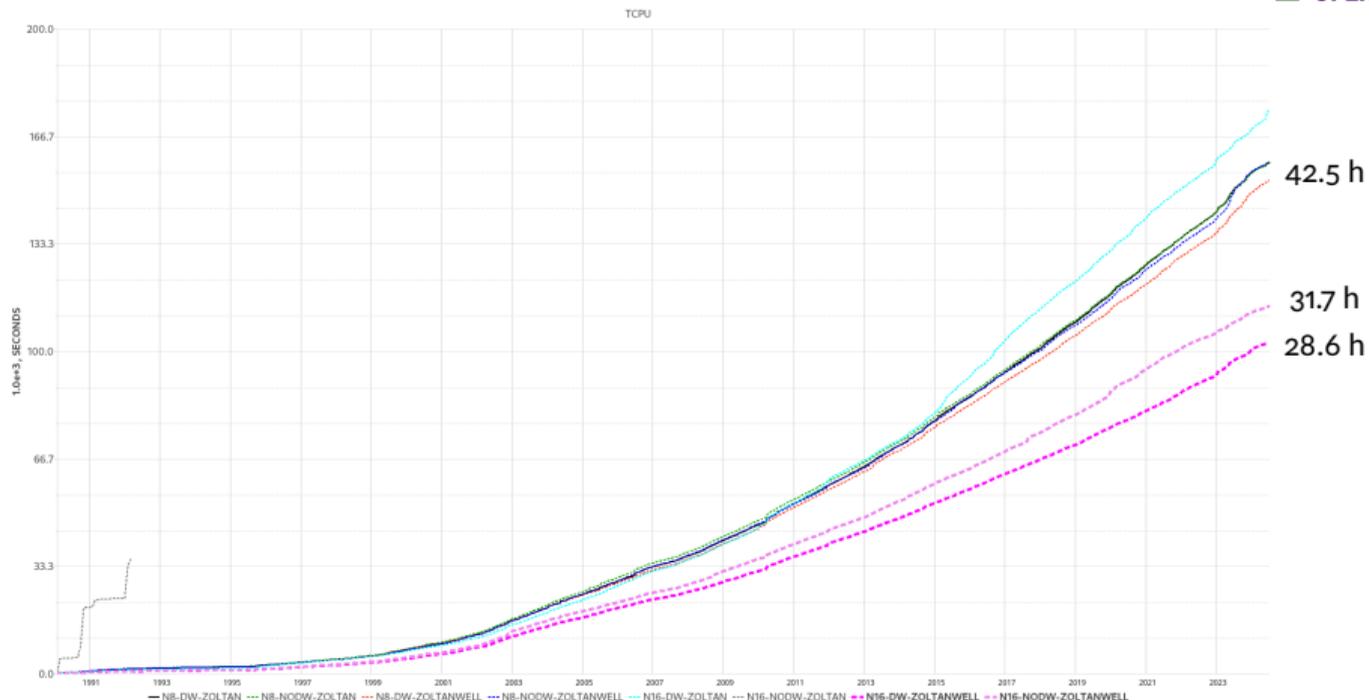
- 8|16 procs, --allow-distributed-wells=true|false --partition-method=zoltan|zoltanwell --allow-splitting-inactive-wells=true  
- Run on a machine with 32 cores, 64 threads, 4.55 GHz max frequency, 128 GB RAM.

# D: opm-tests/norne/NORNE\_ATW2013.DATA



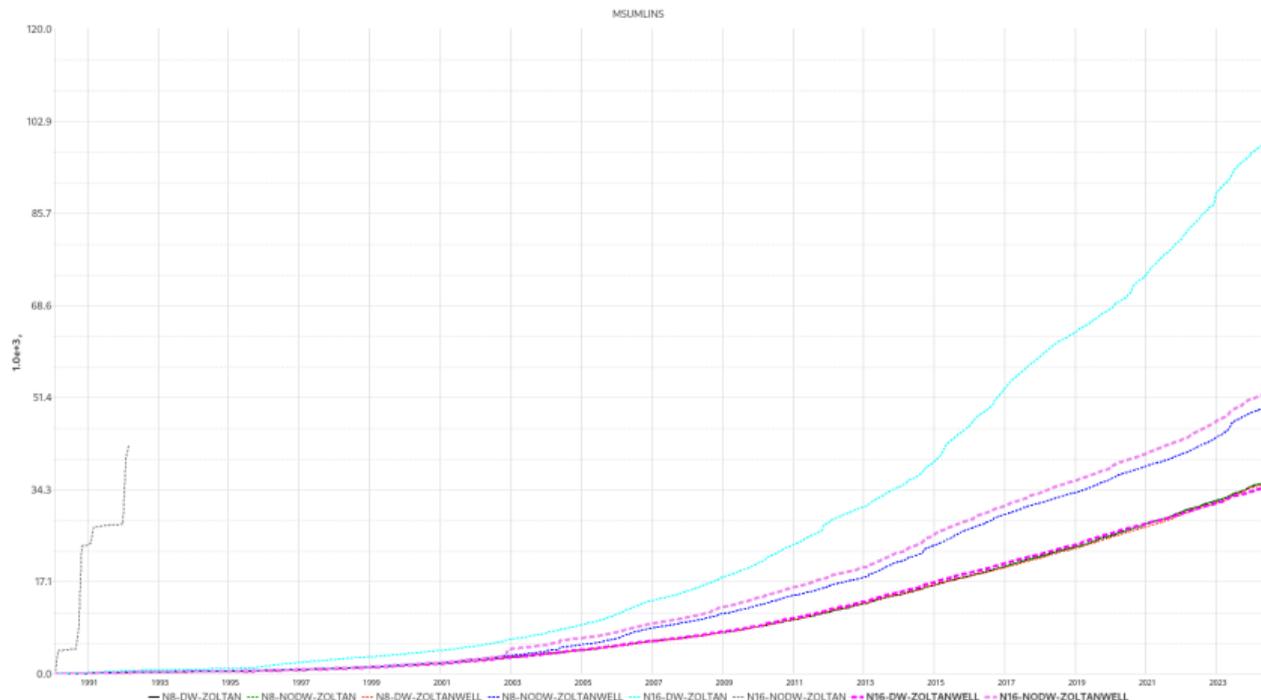
- 8|16 procs, --allow-distributed-wells=true|false --partition-method=zoltan|zoltanwell --allow-splitting-inactive-wells=true  
- Run on a machine with 32 cores, 64 threads, 4.55 GHz max frequency, 128 GB RAM.

# D: Case with $\approx 1.64$ M active cells, 338 active wells



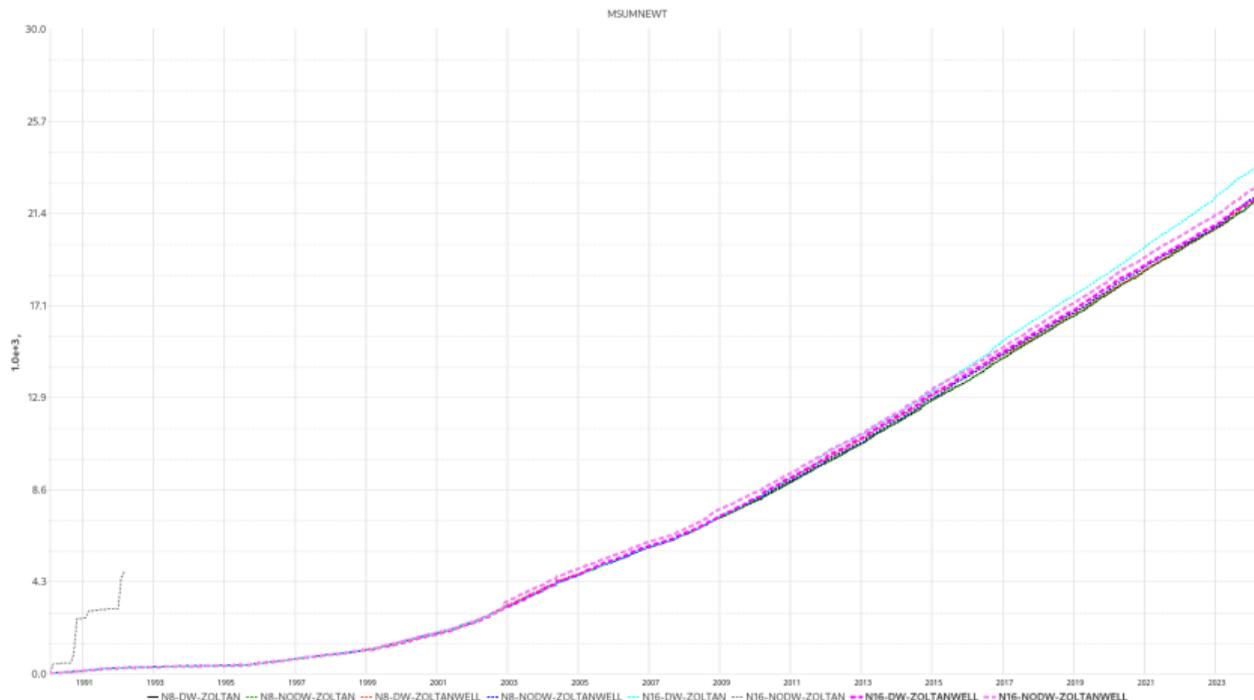
- 8|16 procs, --allow-distributed-wells=true|false --partition-method=zoltan|zoltanwell --allow-splitting-inactive-wells=true  
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## E: Outlook

- Currently works for several test cases, but not for all 😞!
- More thorough verification of correctness needed!
- General problem with distributed wells:

Load balancing distributed the wells as follows:

well name	ranks with perforated cells		
PROD1	0	1	
PROD2	0	1	2
PROD3	0	1	2

→ Careful with throws inside a loop over wells!

- Next steps: alternative solvers or preconditioners for the well equations?
- Many thanks to Markus Blatt, Michal Tóth, Vegard Kippe, Kai Bao and Halvor Møll Nilsen! ❤️